Modeling Dynamic Response of Inverter-Based Resources Using Waveform Measurements

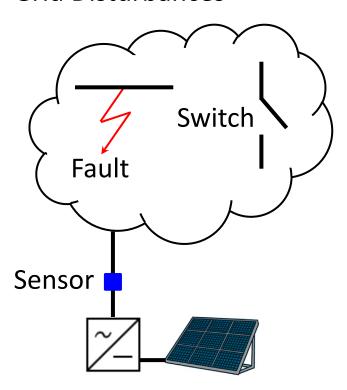
NASPI April Meeting (April 4, 2023)

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Department of Electrical Engineering, University of California, Riverside
Associate Director, Winston Chung Global Energy Center

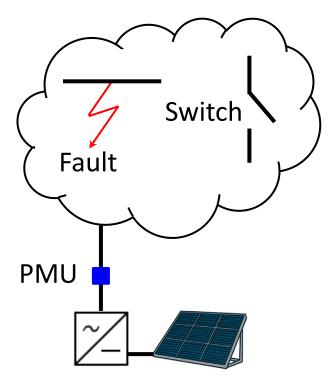
Acknowledgement: Fatemeh Ahmadi (Ph.D. Student)

Grid Disturbances



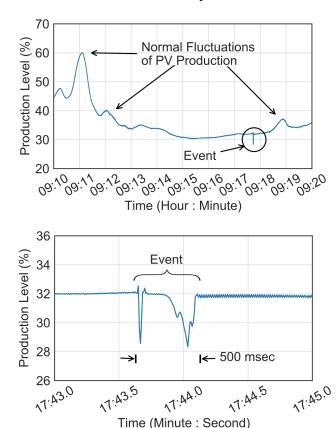
Inverter-Based Resource (IBR)

Grid Disturbances



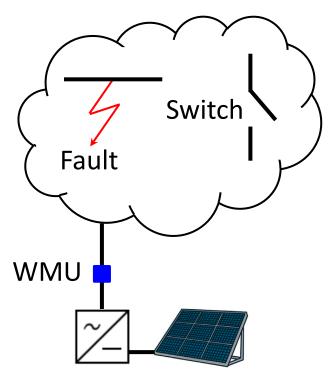
Inverter-Based Resource (IBR)

Phasor-Level Dynamics¹



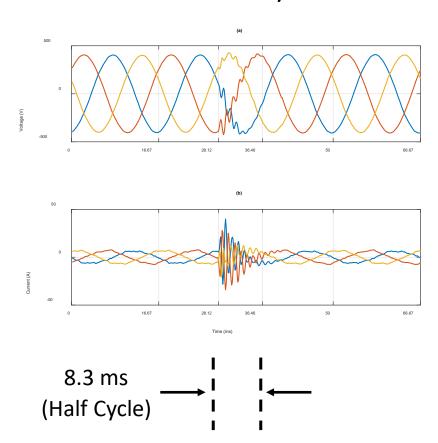
¹ P. Khaledian and H. Mohsenian-Rad, "Automated Event Region Identification and its Data-Driven Applications in Behind-the-Meter Solar Farms Based on Micro-PMU Measurements," in *IEEE Trans. on Smart Grid*, May 2021.

Grid Disturbances

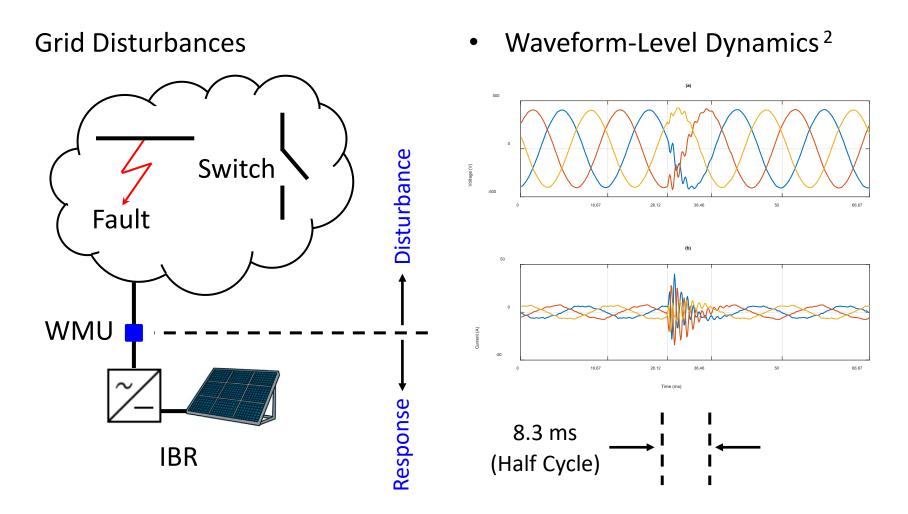


Inverter-Based Resource (IBR)

• Waveform-Level Dynamics²

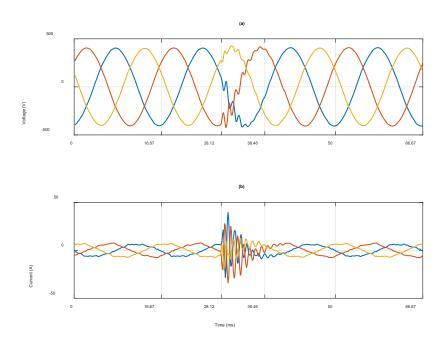


² F. Ahmadi and H. Mohsenian-Rad, "Data-Driven Models for Sub-Cycle Dynamic Response of Inverter-Based Resources Using WMU Measurements," Submitted to *an IEEE Journal* (Under Review), January 2023.



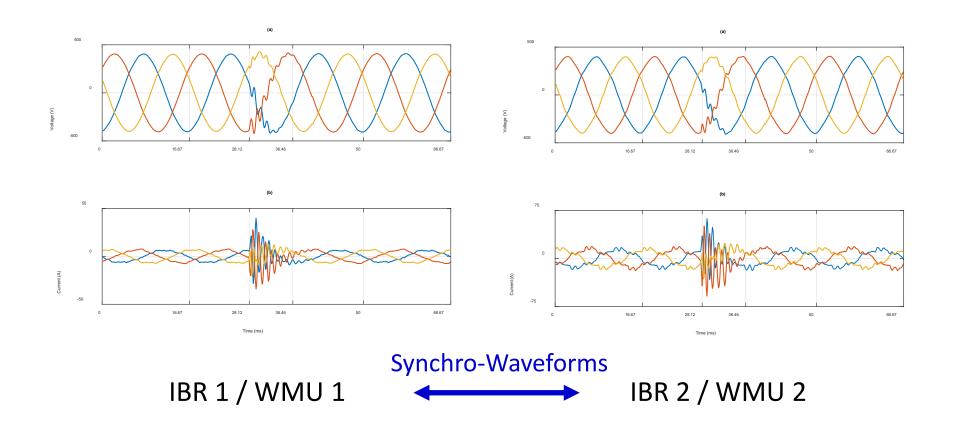
² F. Ahmadi and H. Mohsenian-Rad, "Data-Driven Models for Sub-Cycle Dynamic Response of Inverter-Based Resources Using WMU Measurements," Submitted to *an IEEE Journal* (Under Review), January 2023.

Q: How do we know that this is a "Response" and not the "Cause"?



IBR 1 / WMU 1

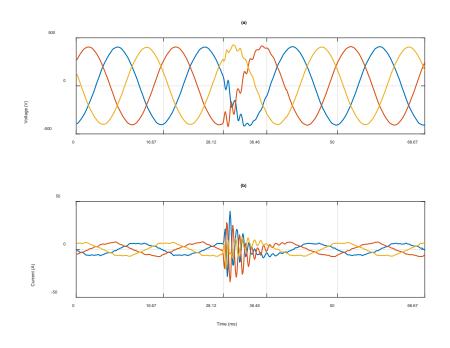
Q: How do we know that this is a "Response" and not the "Cause"?

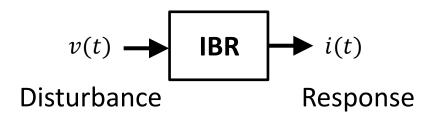


Different Feeders, Similar Inverters, Different Sizes

Modeling Dynamic Response of IBRs

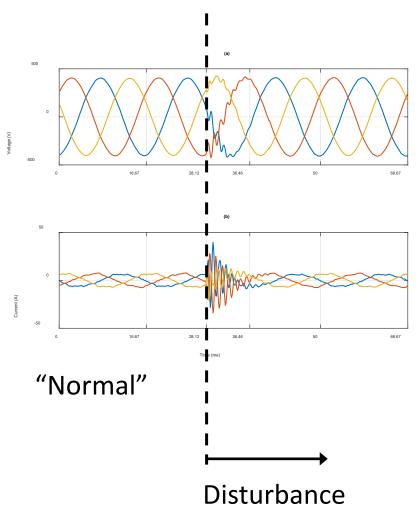
Q: How can we model the IBR's sub-cycle dynamic response?

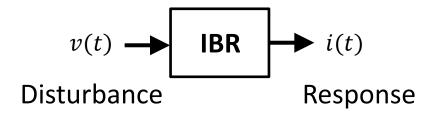




Modeling Dynamic Response of IBRs

Q: How can we model the IBR's sub-cycle dynamic response?

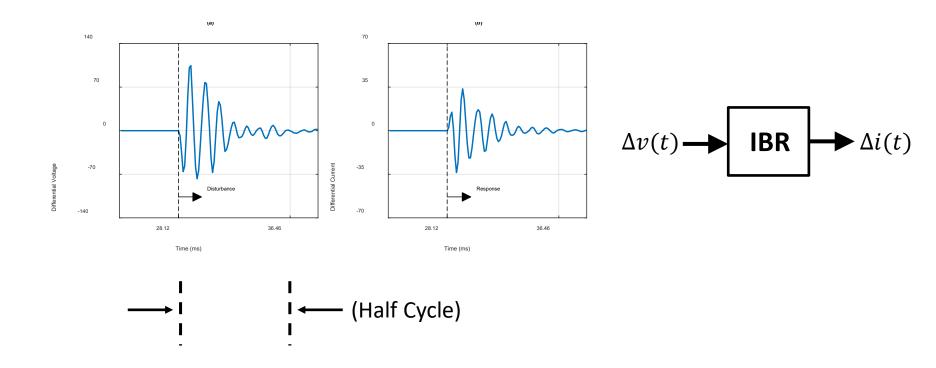




Differential Waveform Dynamics

We use Differential Waveform to obtain the model:

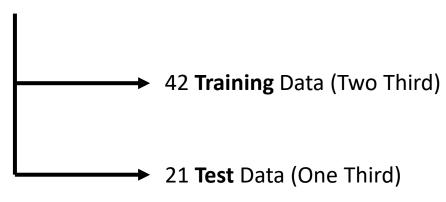
$$\Delta x(t) = x(t) - x_{ref}(x)$$
Normal (e.g., Pre-Disturbance Cycle)



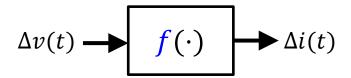
- Field Data Set:
 - PV Unit: 480 V / 100 kW
 - Six Months of WMU Data



63 Disturbances (Differential Voltage and Current Waveforms)



Option 1: Single Model



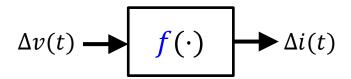
Train $f(\cdot)$ to reach the best match between all 42 pairs of training data:

$$e_1(t) = \Delta i_1(t) - f(\Delta v_1(t))$$

$$e_1(t) = \Delta i_1(t) - f(\Delta v_1(t))$$
 (Same Model)
$$\vdots$$

$$e_{42}(t) = \Delta i_{42}(t) - f(\Delta v_{42}(t))$$

Option 1: Single Model



Train $f(\cdot)$ to reach the best match between all 42 pairs of training data:

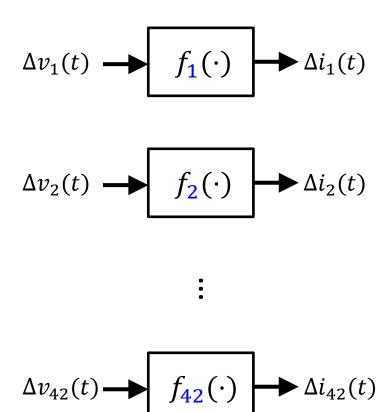
$$e_1(t)=\Delta i_1(t)-f(\Delta v_1(t))$$

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 (Same Model)
$$\vdots$$

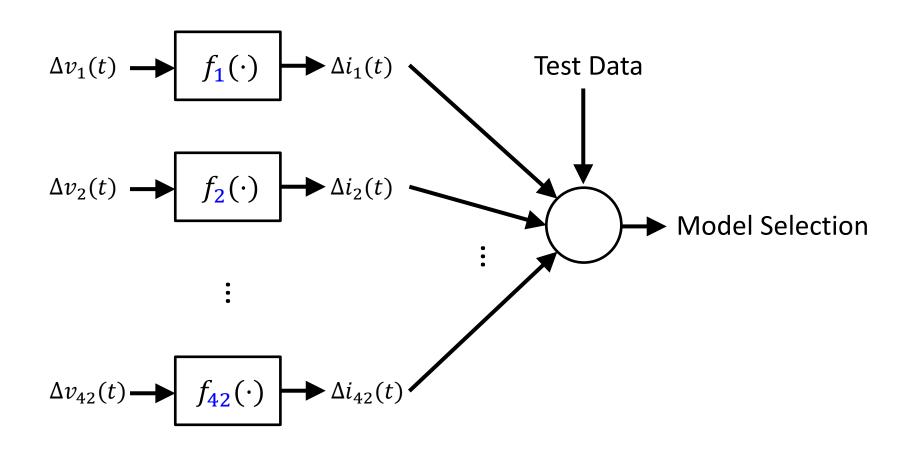
$$e_{42}(t)=\Delta i_{42}(t)-f(\Delta v_{42}(t))$$

Poor Performance!

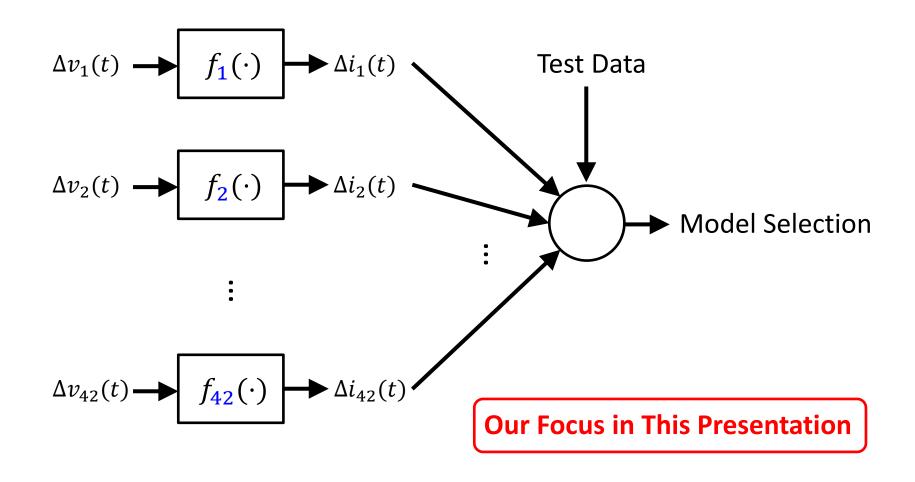
Option 2: Multiple Models



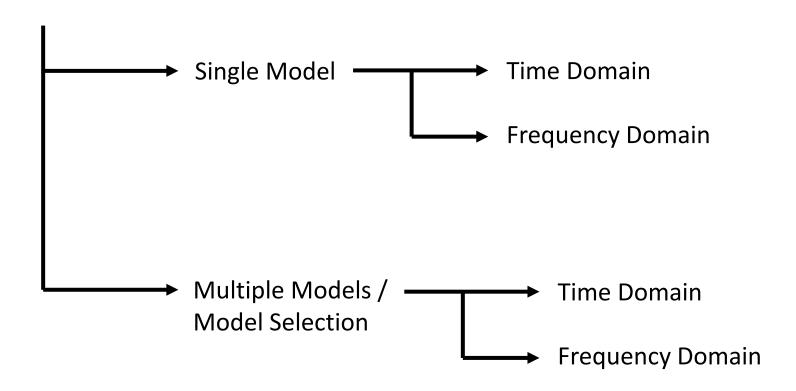
Option 2: Multiple Models



Option 2: Multiple Models

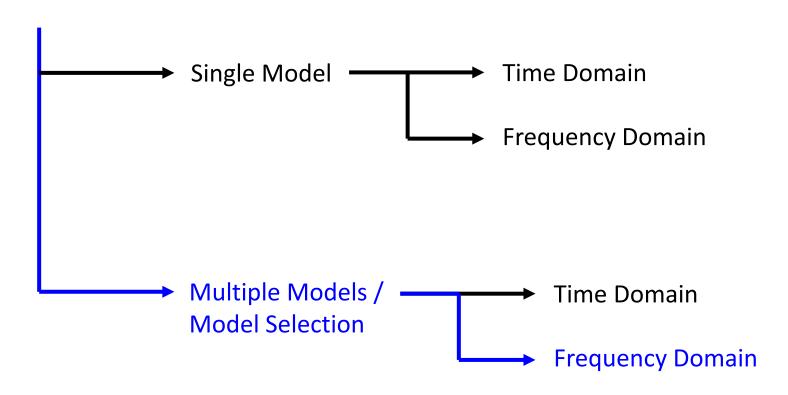


Summary of Options²:



² F. Ahmadi and H. Mohsenian-Rad, "Data-Driven Models for Sub-Cycle Dynamic Response of Inverter-Based Resources Using WMU Measurements," Submitted to *an IEEE Journal* (Under Review), January 2023.

Summary of Options²:



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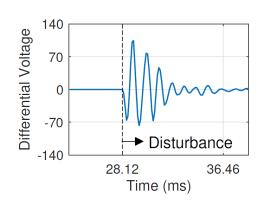
Step 1: Modal Analysis

• Consider one pair of training data: $\Delta v(t)$ and $\Delta i(t)$.

Apply modal analysis (e.g., Prony Method) with M modes to obtain:

$$\Delta v(t) = \sum_{m=1}^{M} A_m e^{\sigma_m t} \cos(\omega_m t + \phi_m),$$

$$\Delta i(t) = \sum_{m=1}^{M} B_m e^{\sigma_m t} \cos(\omega_m t + \psi_m),$$



• At dynamic each mode m, we can define the equivalent admittance of the IBR at that particular mode $z_m = \sigma_m + j\omega_m$ as the following complex number:

$$\mathbf{H}_m = \frac{B_m \angle \psi_m}{A_m \angle \phi_m} = \frac{B_m}{A_m} \angle (\psi_m - \phi_m) \quad \text{at} \quad \sigma_m + j\omega_m.$$

Step 2: Library Construction

• Now consider all the K = 42 pairs of training data.

• We can construct a *library* of $K \times M$ dynamic models:

$$\mathbf{H}_m^k$$
 at $z_m^k = \sigma_m^k + j\omega_m^k$, $k = 1, \dots, K, m = 1, \dots, M.$

• Each model corresponds to **one** dynamic mode that is derived from **one** disturbance; thus adding up to $K \times M$ models using modal analysis.

Step 3: Model Selection

• Let $\Delta v_{\text{test}}(t)$ and $\Delta i_{\text{test}}(t)$ denote the differential voltage and the differential current waveform for a given test disturbance.

Apply modal analysis to the input test signal:

$$\Delta v_{\rm test}(t)$$
 — Dynamic Modes: $z_{n,\rm test} = \sigma_{n,\rm test} + j\omega_{n,\rm test}$

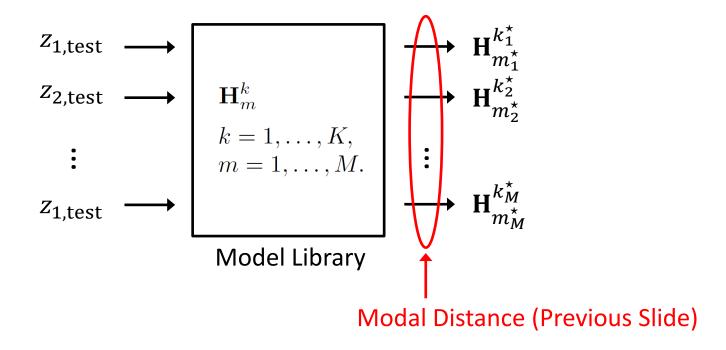
For any such dynamic mode n, we obtain (based on input-voltage):

$$[k_n^{\star}, m_n^{\star}] = \underset{k,m}{\operatorname{arg\,min}} |z_{n,\text{test}} - z_m^k|^2.$$

(Minimum *Model* Distance)

Step 3: Model Selection (Cont.)

Accordingly, we obtain n models corresponding to the n modes:



Step 4: Dynamic Response Estimation

- Given $\mathbf{H}_{m_1^{\star}}^{k_1^{\star}}$, $\mathbf{H}_{m_2^{\star}}^{k_2^{\star}}$, \cdots , $\mathbf{H}_{m_M^{\star}}^{k_M^{\star}}$ for each test input voltage signal $\Delta v_{\mathrm{test}}(t)$.
- We estimate the output signal $\Delta i_{\text{test}}(t)$ as follows:

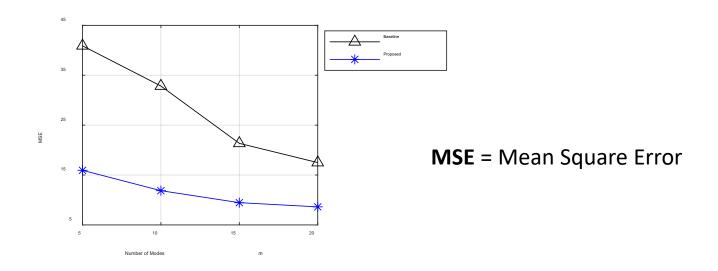
$$\hat{\Delta}i_{\text{test}}(t) = \sum_{n=1}^{M} C_n e^{\sigma_{n,\text{test}}t} \cos(\omega_{n,\text{test}}t + \varphi_n),$$

where

$$C_n = A_{n,\text{test}} \left| \mathbf{H}_{m_n^{\star}}^{k_n^{\star}} \right|, \quad \varphi_n = \phi_{n,\text{test}} + \angle \mathbf{H}_{m_n^{\star}}^{k_n^{\star}}.$$

Some Experimental Results

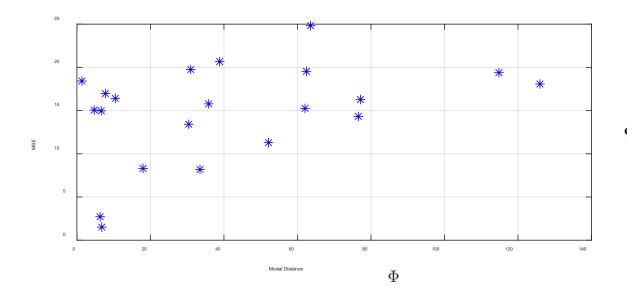
- Results best on 21 Test Disturbances (Out-of-Sample Tests)
- Baseline method: Single Model Approach



Additional modes improve performance (bigger library).

Some Experimental Results

Impact of Modal Distance (of Individual Test Samples):

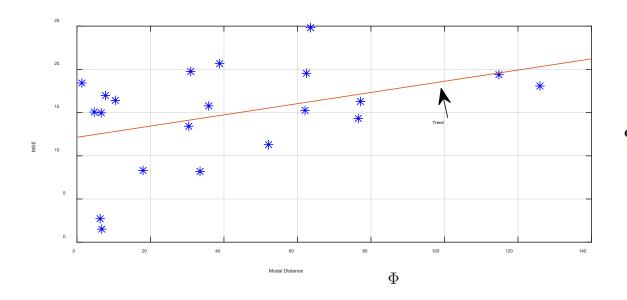


$$\Phi = \sqrt{\sum_{n=1}^{M} \left| z_{n,\text{test}} - z_{m_n^{\star}}^{k_n^{\star}} \right|^2}$$

Shorter modal distance (from library) leads to better output estimation.

Some Experimental Results

Impact of Modal Distance (of Individual Test Samples):



$$\Phi = \sqrt{\sum_{n=1}^{M} \left| z_{n,\text{test}} - z_{m_n^{\star}}^{k_n^{\star}} \right|^2}$$

Shorter modal distance (from library) leads to better output estimation.

Some Potential Use Cases

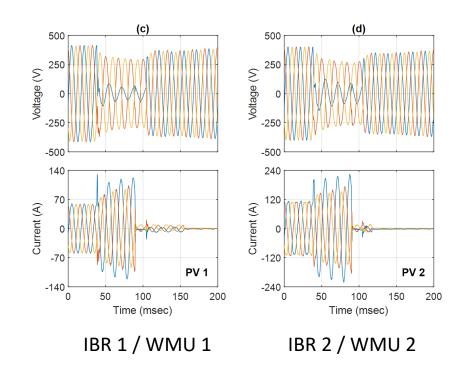
• 1) Dynamic Analysis of Individual IBRs (Diagnosis, Trip Prediction, etc.)

2) Comparing Dynamic Response of IBRs (Synchro-Waveforms)

• 3) Aggregate Dynamic Response

• 4) Potential Ripple Effects

5) Other (To be Explored)



Further Reading

WMU-Based Dynamic Load Modeling (Will be Published Soon):

F. Ahmadi and H. Mohsenian-Rad, "Data-Driven Models for Sub-Cycle Dynamic Response of Inverter-Based Resources Using WMU Measurements," *Submitted to an IEEE Journal* (Under Review), January 2023.

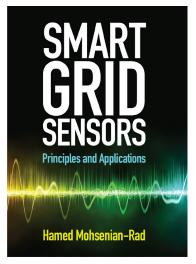
WMUs and Synchro-Waveforms:

[1] M. Izadi and H. Mohsenian-Rad, "Characterizing synchronized Lissajous curves to scrutinize power distribution synchro-waveform measurements," in *IEEE Trans. on Power Systems*, vol. 36, no. 5, p. 4880, Sept 2021.

[2] M. Izadi and H. Mohsenian-Rad, "Synchronized Lissajous-based method to detect & classify events in synchro-waveform measurements in power distribution networks," in *IEEE Trans. on Smart Grid*, vol. 13, May 2022.

[3] M. Izadi and H. Mohsenian-Rad, "synchronous waveform measurements to locate transient events and incipient faults in power distribution networks," in *IEEE Trans. on Smart Grid*, vol. 12, no. 5, pp. 4295, Sept 2021.

Chapter 4



Cambridge University Press, April 2022

Thank You!

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