

# **Interaction of Forced Oscillation with Multiple System Modes**

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- Rough zone operation of certain hydro units (Francis turbines)
- Mechanical control failures (valves)
- Power electronics control issues (wind,solar,HVDC)
- Poor or incorrect designs (operation outside design range)
- Problematic loads: arc furnaces, oil refineries

# Forced Oscillations

- Signature: Sudden appearance and end of oscillations (not related to grid events)
- Mechanism: Root cause external to power grid operations
- Warning signs: Not much. Problem tends to repeat itself until corrected.
- Challenge: Effects are local usually. Can lead to **wide-area oscillations** sometimes from **inter-area resonance**.

**Resonance effect high** when:

- (R1) Forced Osc freq near System Mode freq
- (R2) System Mode poorly damped
- (R3) Forced Oscillation location near distant ends (strong participation) of the System Mode

**Resonance effect medium** when:

- Some of the conditions hold

**Resonance effect small** when:

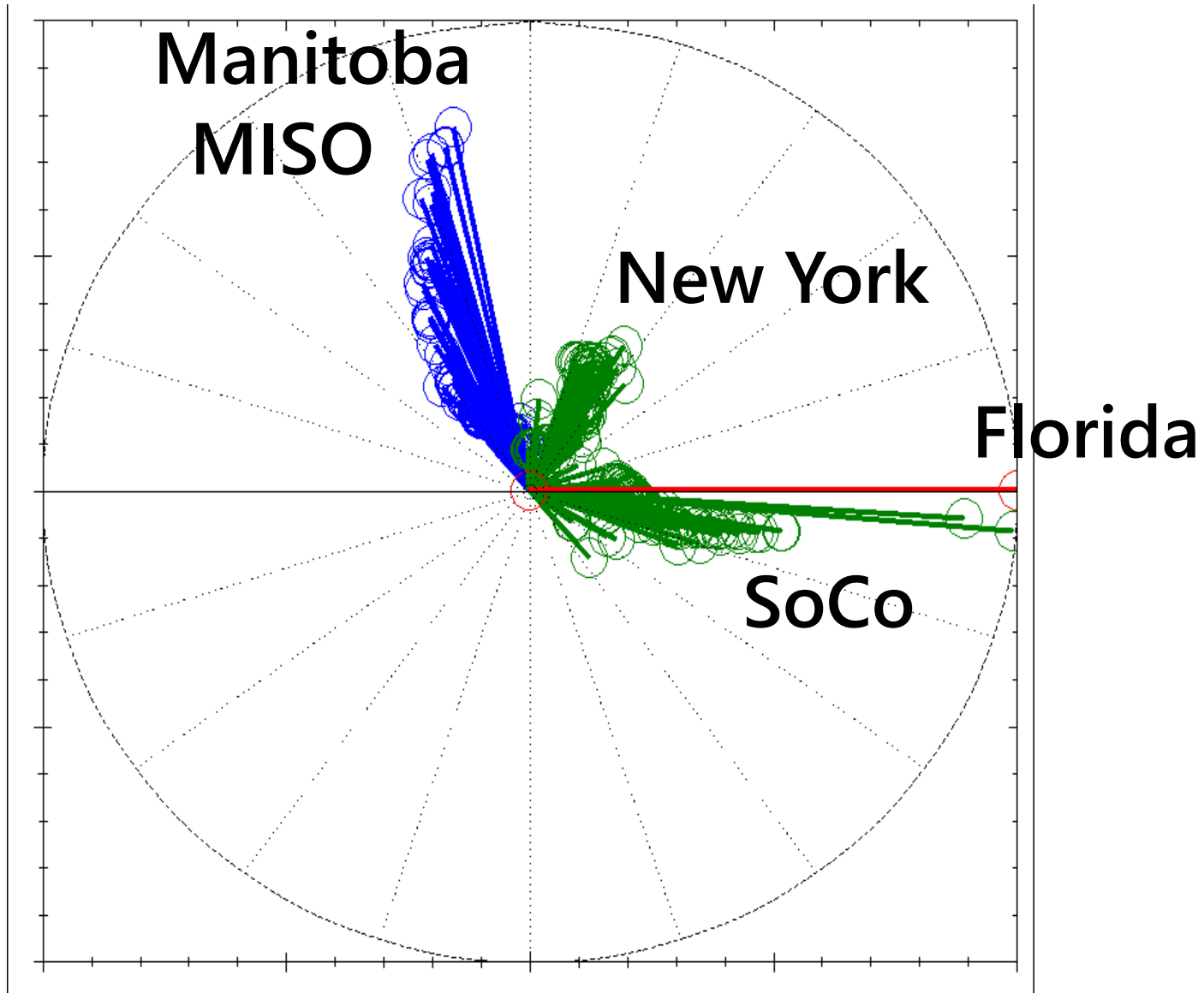
- None of the condition holds

S.A.N. Sarmadi and V. Venkatasubramanian, "Inter-Area Resonance in Power Systems From Forced Oscillations," *IEEE Trans. Power Systems*, vol.31, no.1, pp.378-386, Jan. 2016.

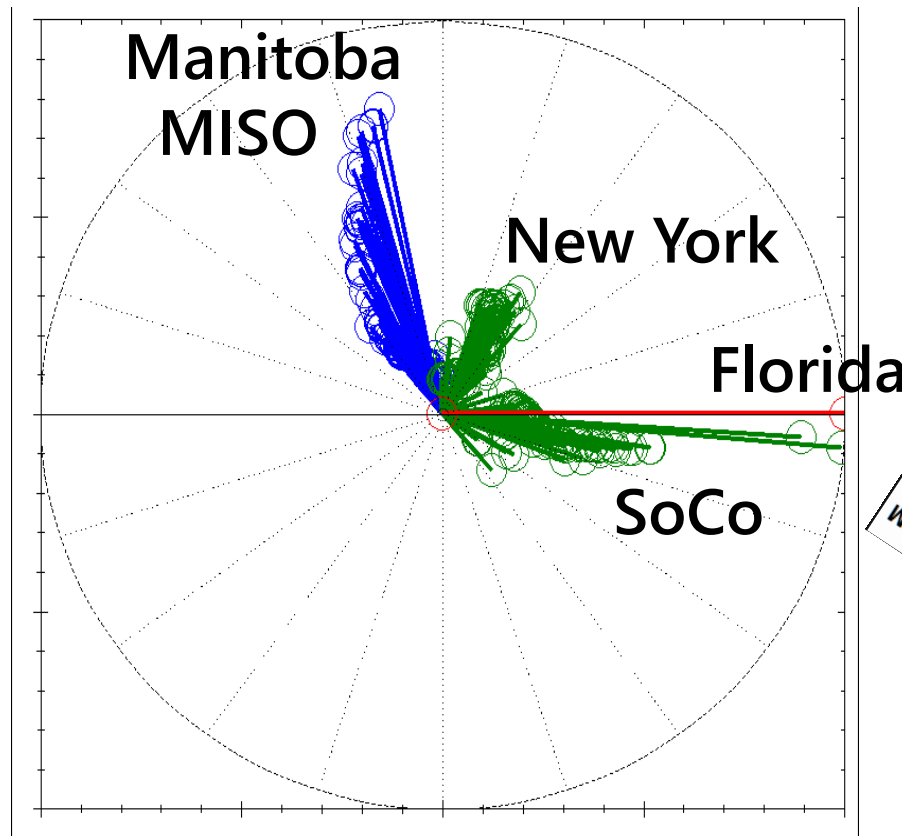




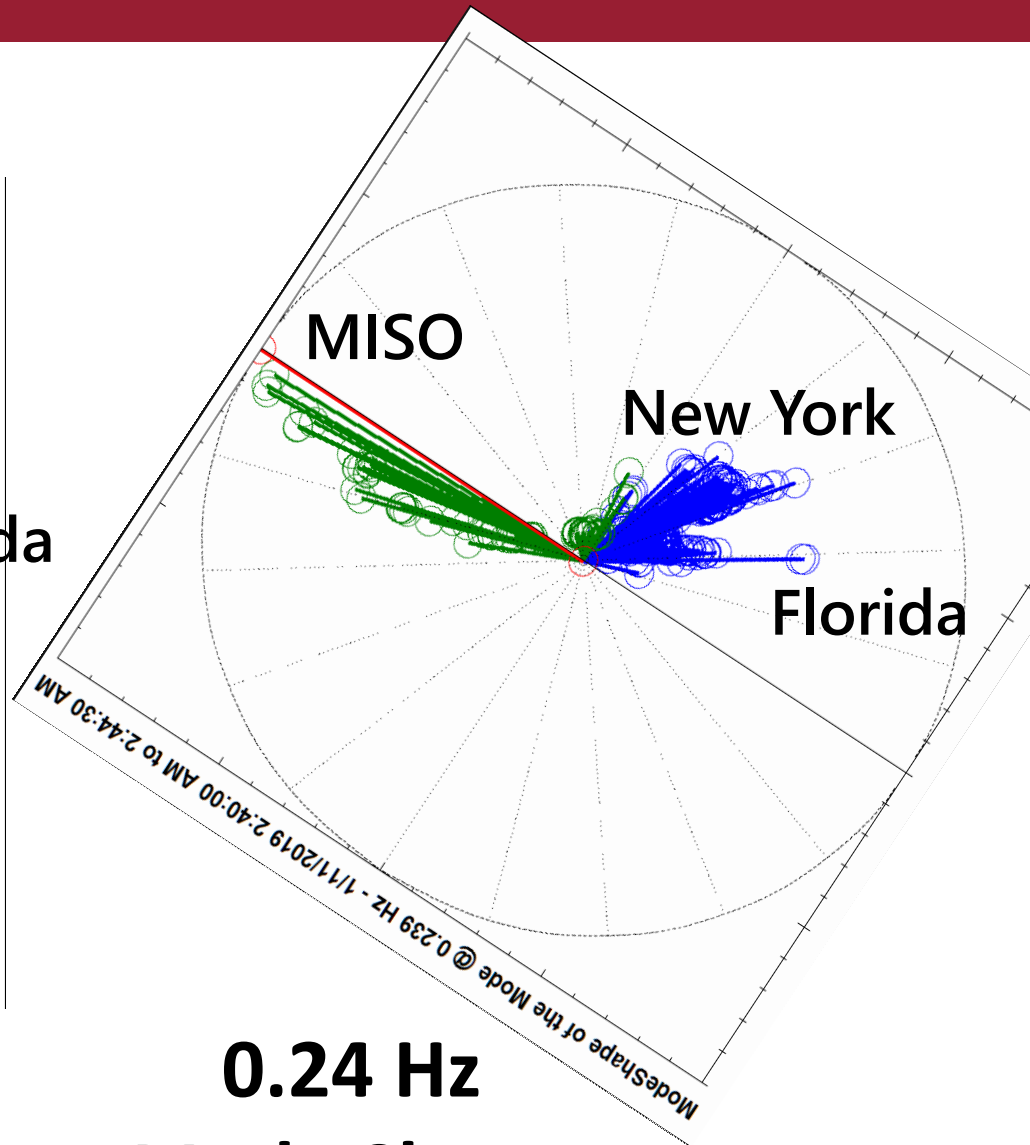
# 0.25 Hz Oscillation Shape



# 0.25 Hz Oscillation Shape Comparison



**0.25 Hz  
Oscillation Shape**



**0.24 Hz  
Mode Shape**

# Oscillation Shape Proposition

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{b}u, \quad u(t) = H \cos(\omega t + \gamma)$$

Sinusoidal steady state:

$$x_i(t) = A_{FR_i} \cos(\omega t + \Psi_{FR_i})$$

$$\mathbf{A}_{FR} \angle \mathbf{\Psi}_{FR} = -(H \angle \gamma) \left( \sum_{i=1}^{2n_c} \tilde{\mathbf{v}}_i \frac{|\tilde{\mathbf{w}}_i^T \mathbf{b}|}{\sqrt{\alpha_i^2 + (\omega - \beta_i)^2}} [\angle(\tilde{\mathbf{w}}_i^T \mathbf{b}) + \angle(\alpha_i + j(\omega - \beta_i))] \right. \\ \left. + \sum_{i=2n_c+1}^n \tilde{\mathbf{v}}_i \frac{|\tilde{\mathbf{w}}_i^T \mathbf{b}|}{\sqrt{\lambda_i^2 + \omega^2}} [\angle(\tilde{\mathbf{w}}_i^T \mathbf{b}) + \angle(\lambda_i + j\omega)] \right)$$

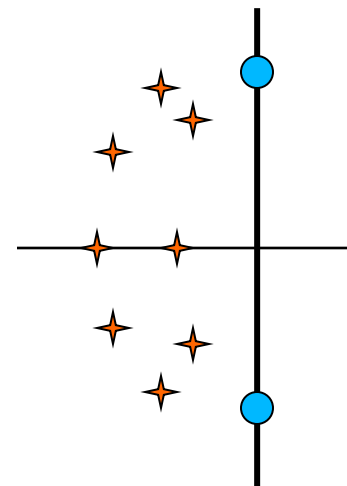
Y. Zhi and V. Venkatasubramanian, "Interaction of Forced Oscillation With Multiple System Modes," *IEEE Trans. Power Systems*, vol. 36, no. 1, pp. 518-520, Jan. 2021.

# Oscillation Shape Proposition

Oscillation shape is a **weighted sum** of mode shapes from all system modes.

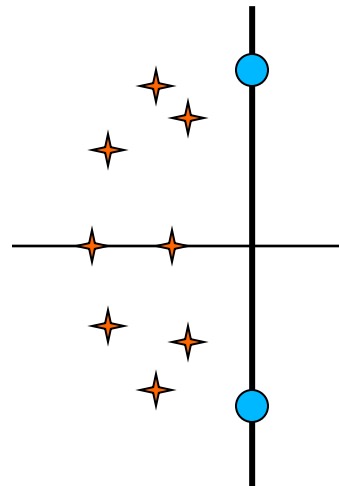
Each mode  $\alpha_i + j\beta_i$  contributes its mode shape  $\tilde{\mathbf{v}}_i$  multiplied by amplification factor  $A_i$  and shifted by rotation factor  $\psi_i$

$$A_i = - \frac{|\tilde{\mathbf{w}}_i^T \mathbf{b}|}{\sqrt{\alpha_i^2 + (\omega - \beta_i)^2}}$$



# Modal Amplification Factors

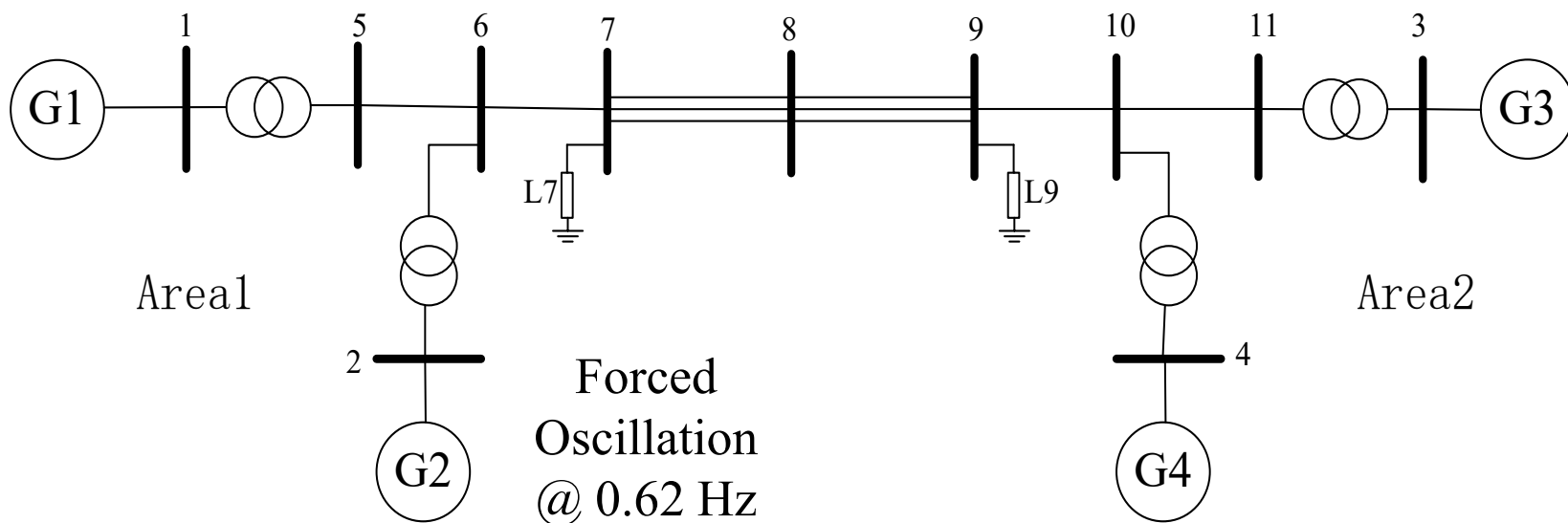
$$|A_i| = \frac{|\tilde{\mathbf{w}}_i^T \mathbf{b}|}{\sqrt{\alpha_i^2 + (\omega - \beta_i)^2}}$$



- $\tilde{\mathbf{w}}_i^T \mathbf{b} \Rightarrow$  Strong controllability (R3)
- $\omega \approx \beta_i \Rightarrow$  Close frequencies (R1)
- $\alpha_i$  small  $\Rightarrow$  Poor damping (R2)

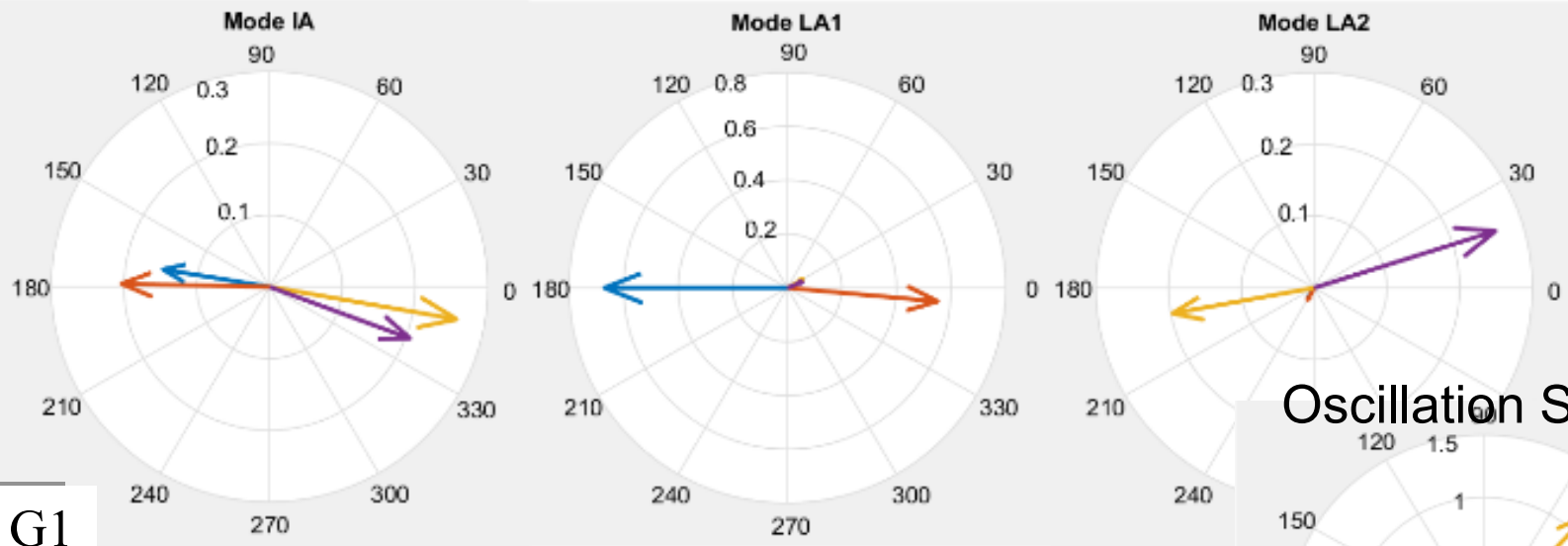
Y. Zhi and V. Venkatasubramanian, "Interaction of Forced Oscillation With Multiple System Modes," *IEEE Trans. Power Systems*, vol.36, no.1, pp.518-520, Jan. 2021.

# Kundur System Example



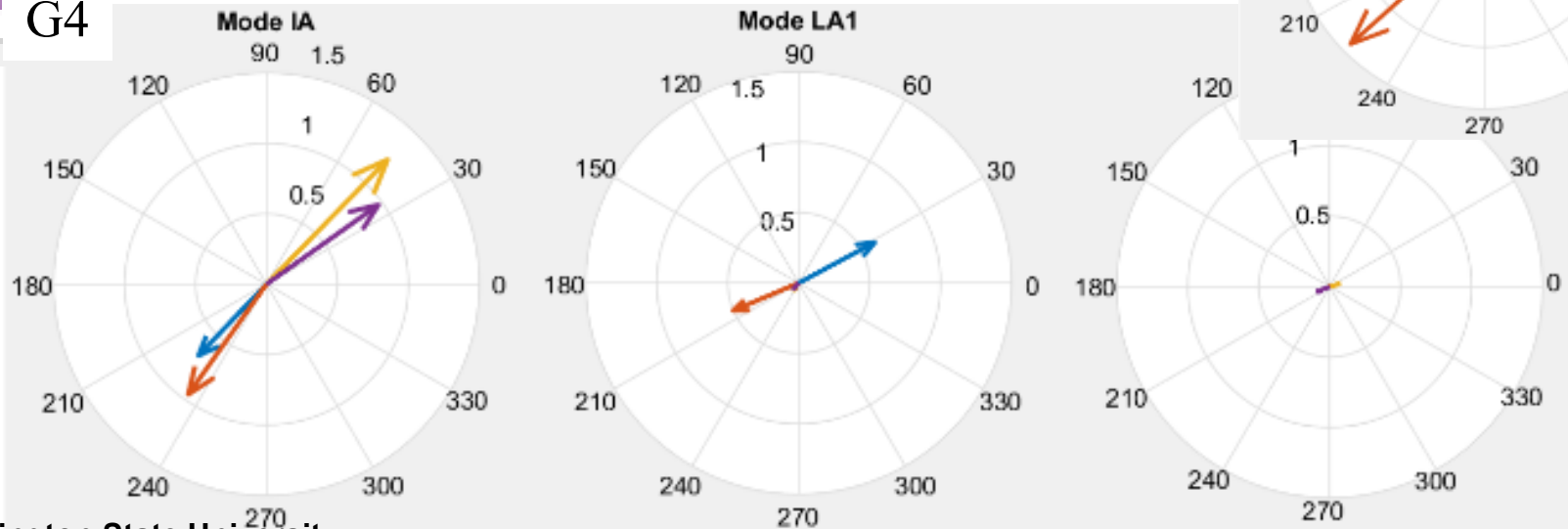
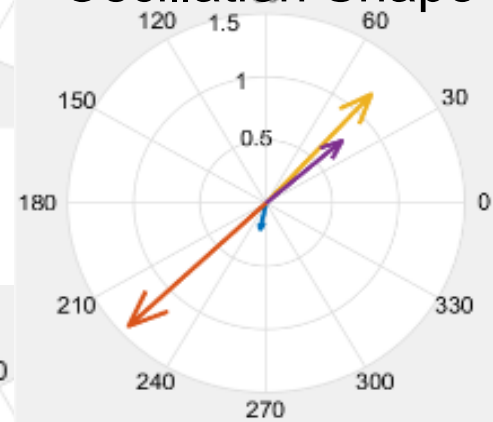
	Type	Frequency	Damping Ratio	$A_i \angle \psi_i$
Mode IA	Inter-area	0.62 Hz	3.0%	$4.70 \angle 56.0^\circ$
Mode LA1	Local (Area1)	0.56 Hz	6.8%	$0.91 \angle -151.7^\circ$
Mode LA2	Local (Area2)	0.67 Hz	1.4%	$0.36 \angle 174.7^\circ$

# Mode shapes



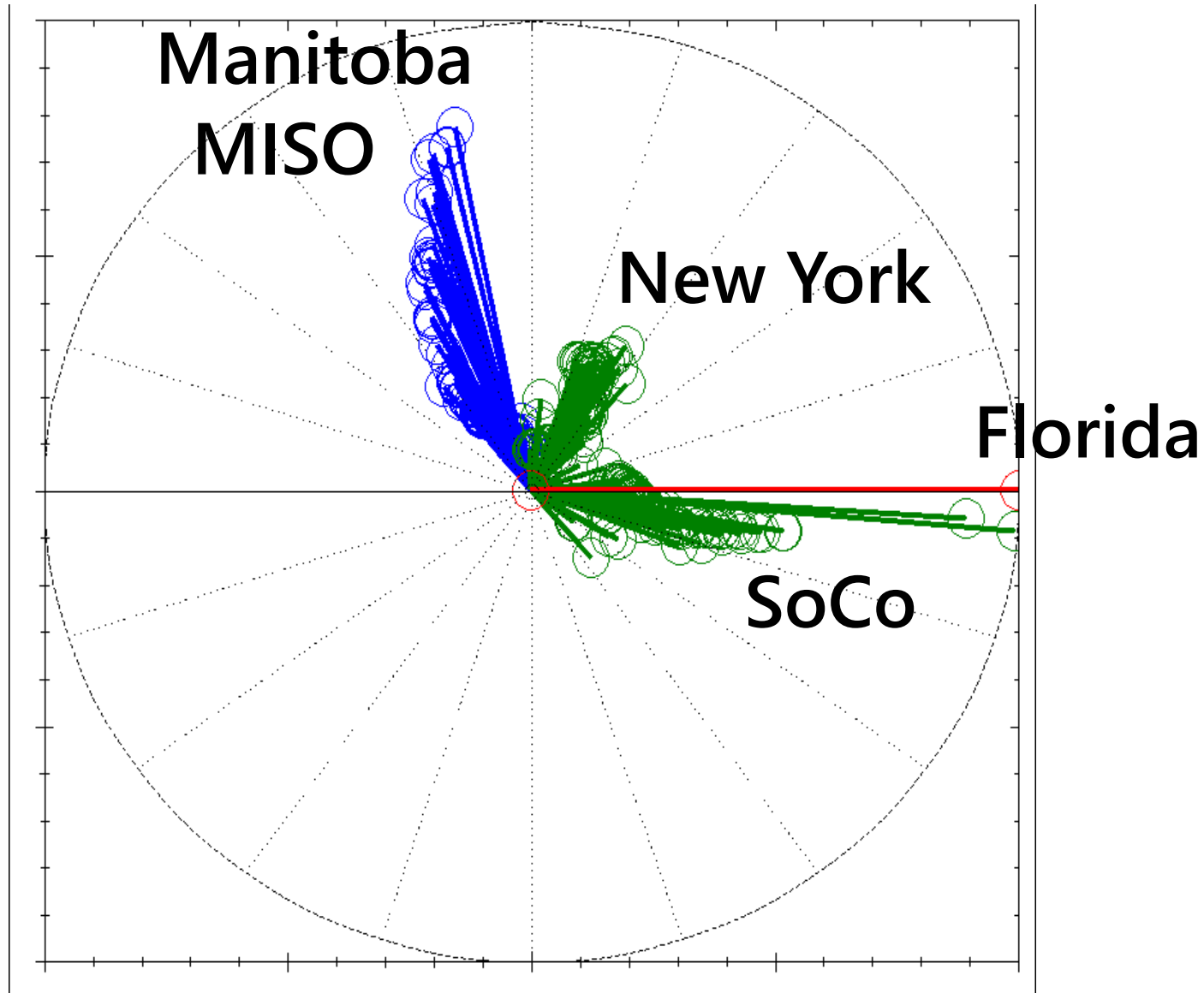
## Modal Contributions

Oscillation Shape

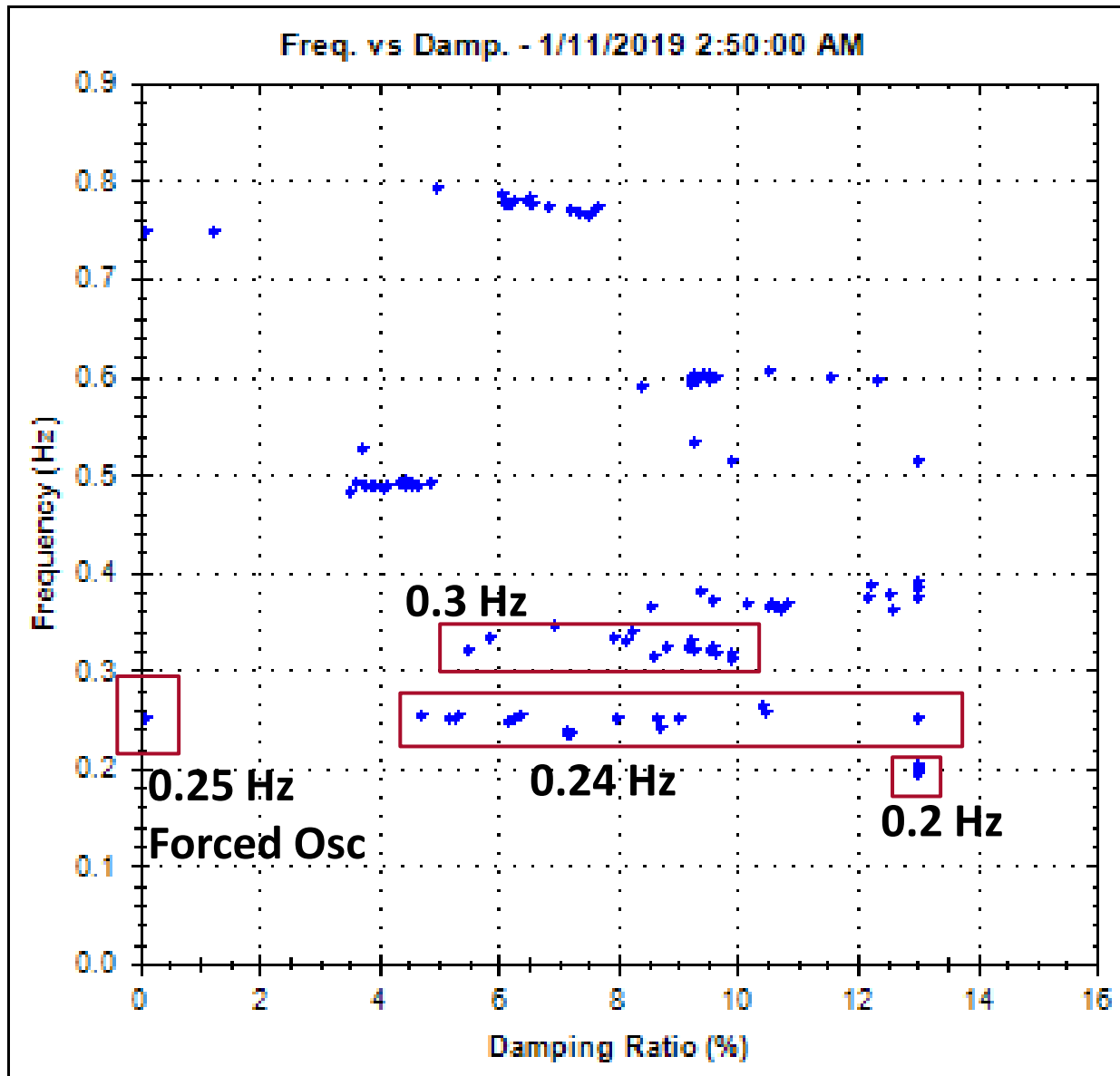




# 0.25 Hz Oscillation Shape



# FSSI Analysis During Event



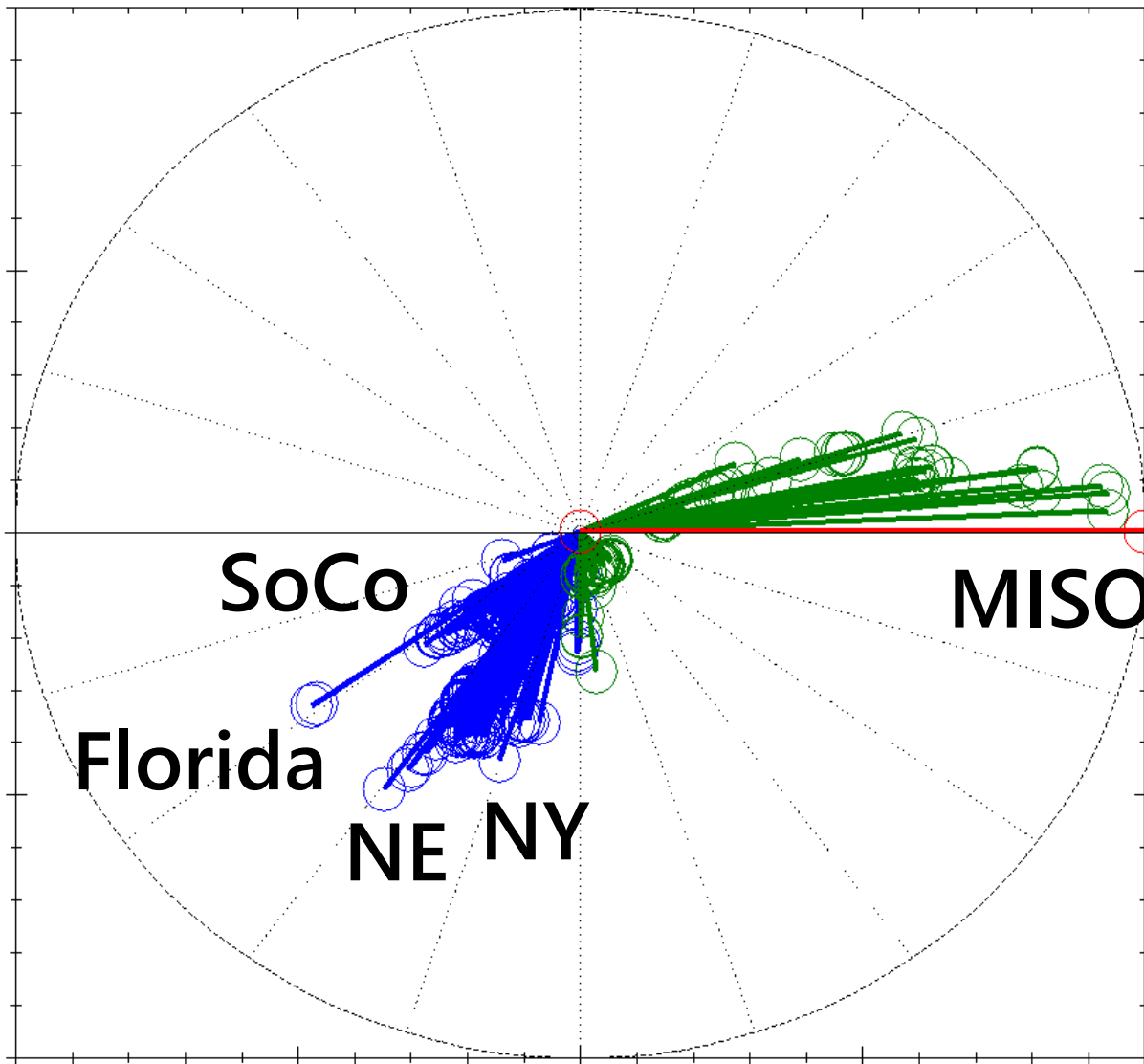
**FSSI Analysis.**  
**442 signals.**

**0.24 Hz mode**  
**excited by**  
**0.25 Hz forced**  
**oscillation.**

**0.24 Hz and**  
**0.3 Hz active.**  
**0.2 Hz inactive.**

# 0.24 Hz NE-NW-SE Mode Shape

ModeShape of the Mode @ 0.239 Hz - 1/11/2019 2:40:00 AM to 2:44:30 AM



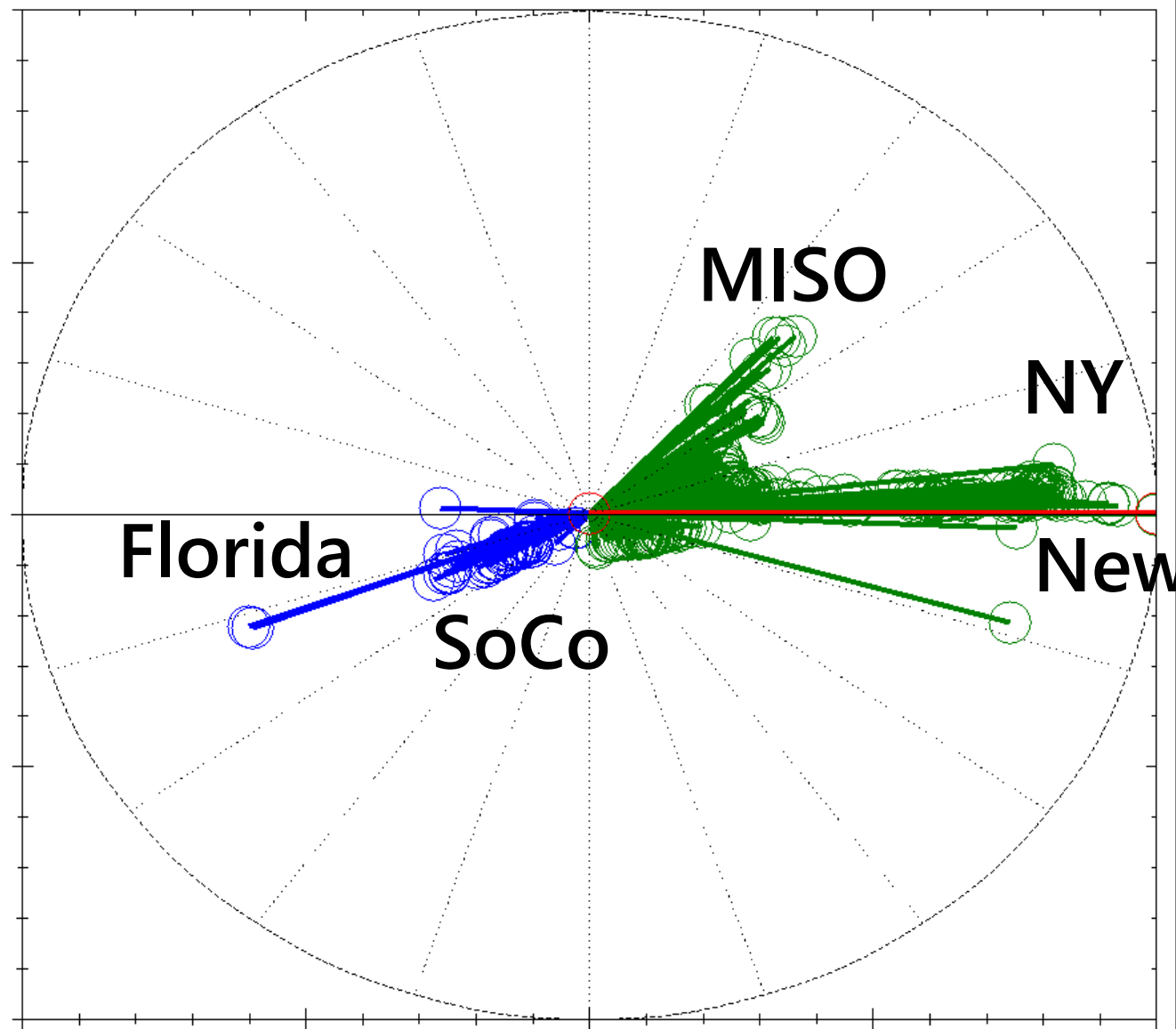
**0.24 Hz mode**

**10.1%**  
**Damping ratio**

**NE-NW-SE**  
**mode**

# 0.2 Hz N-S Mode Shape

ModeShape of the Mode @ 0.201 Hz - 1/11/2019 2:40:00 AM to 2:44:30 AM



0.2 Hz mode

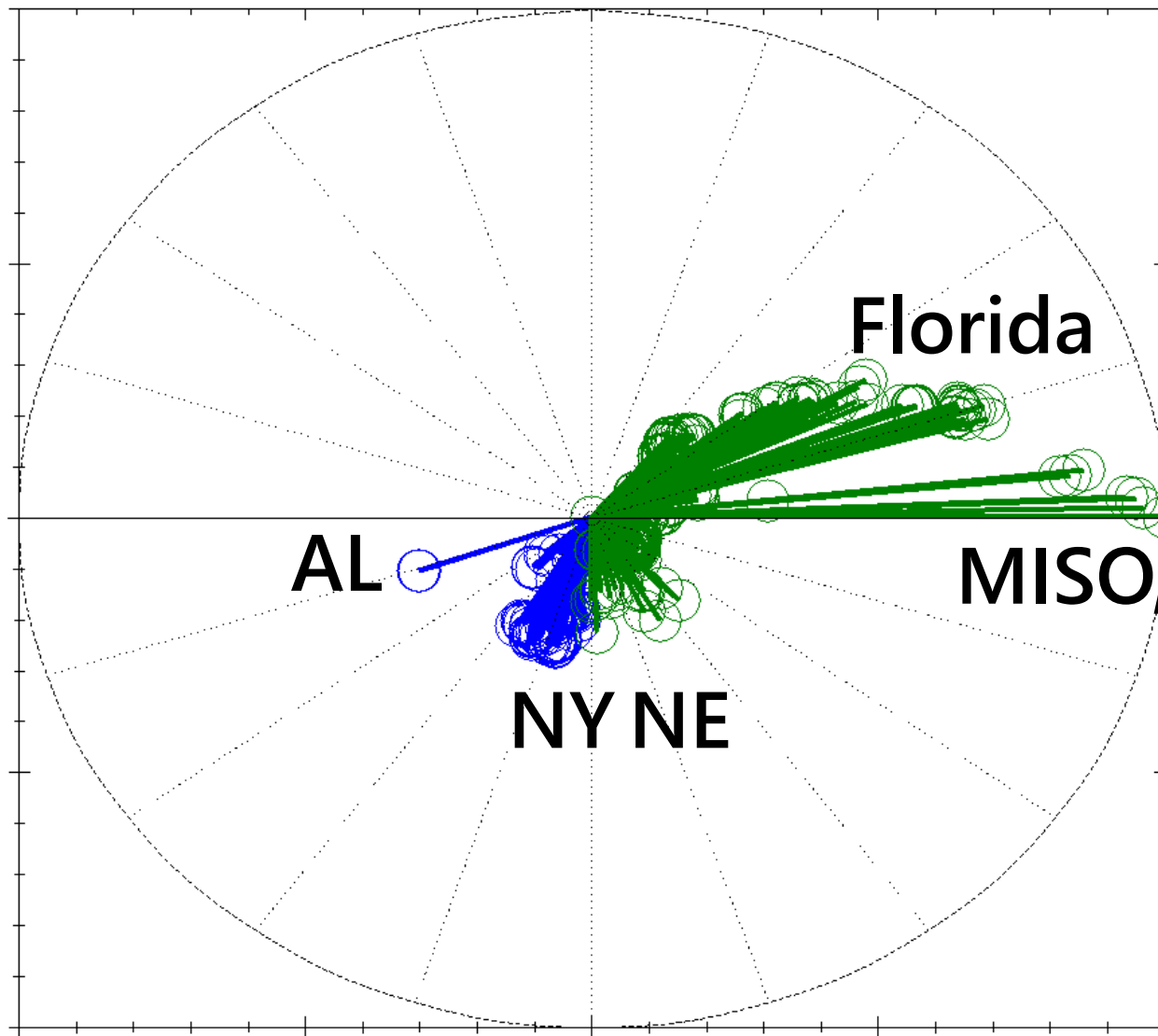
10.9%  
Damping ratio

North-South  
mode

New Eng

# 0.3 Hz Mode Shape

ModeShape of the Mode @ 0.326 Hz - 1/11/2019 2:45:30 AM to 2:50:00 AM



0.3 Hz mode

8.6% Damping  
ratio

North-South  
mode

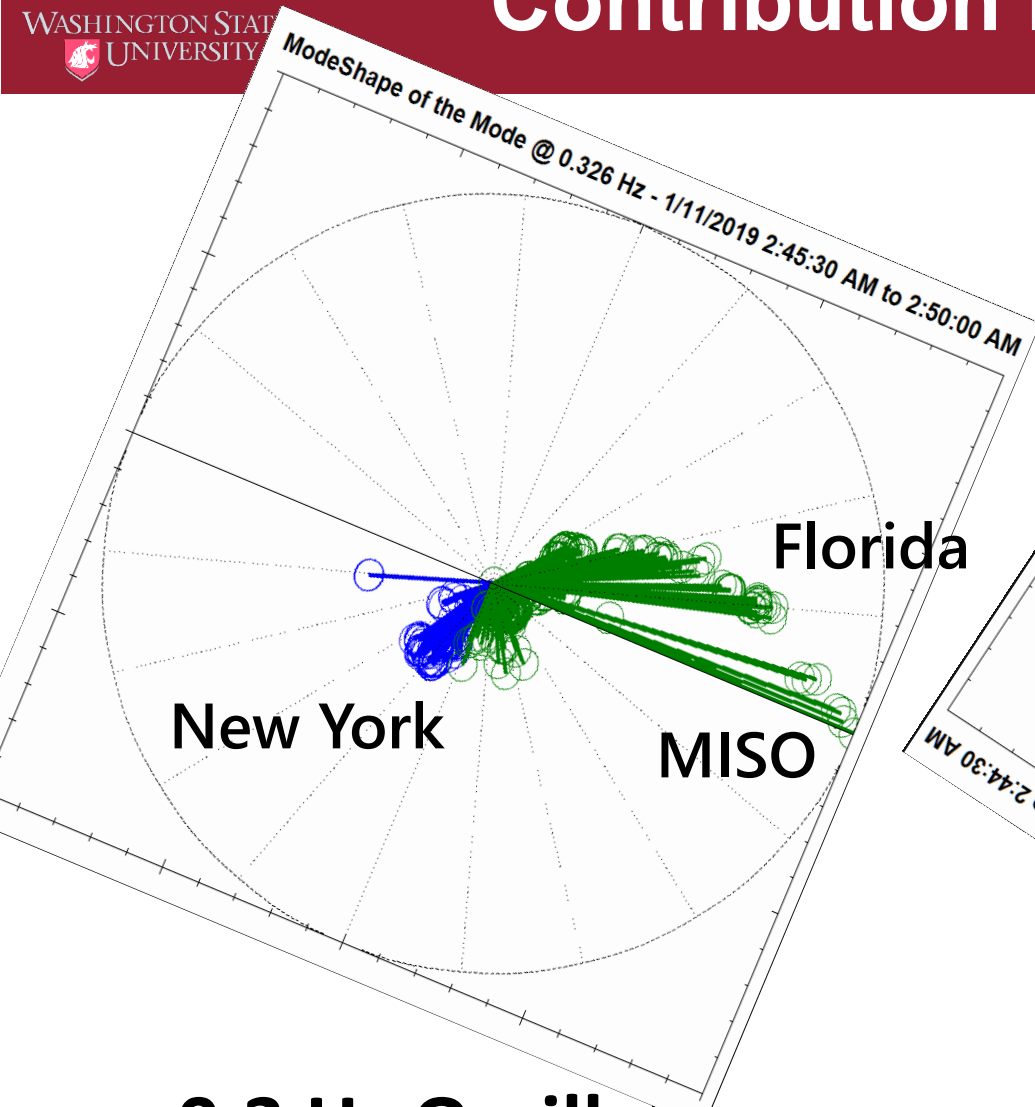
AL

NY NE

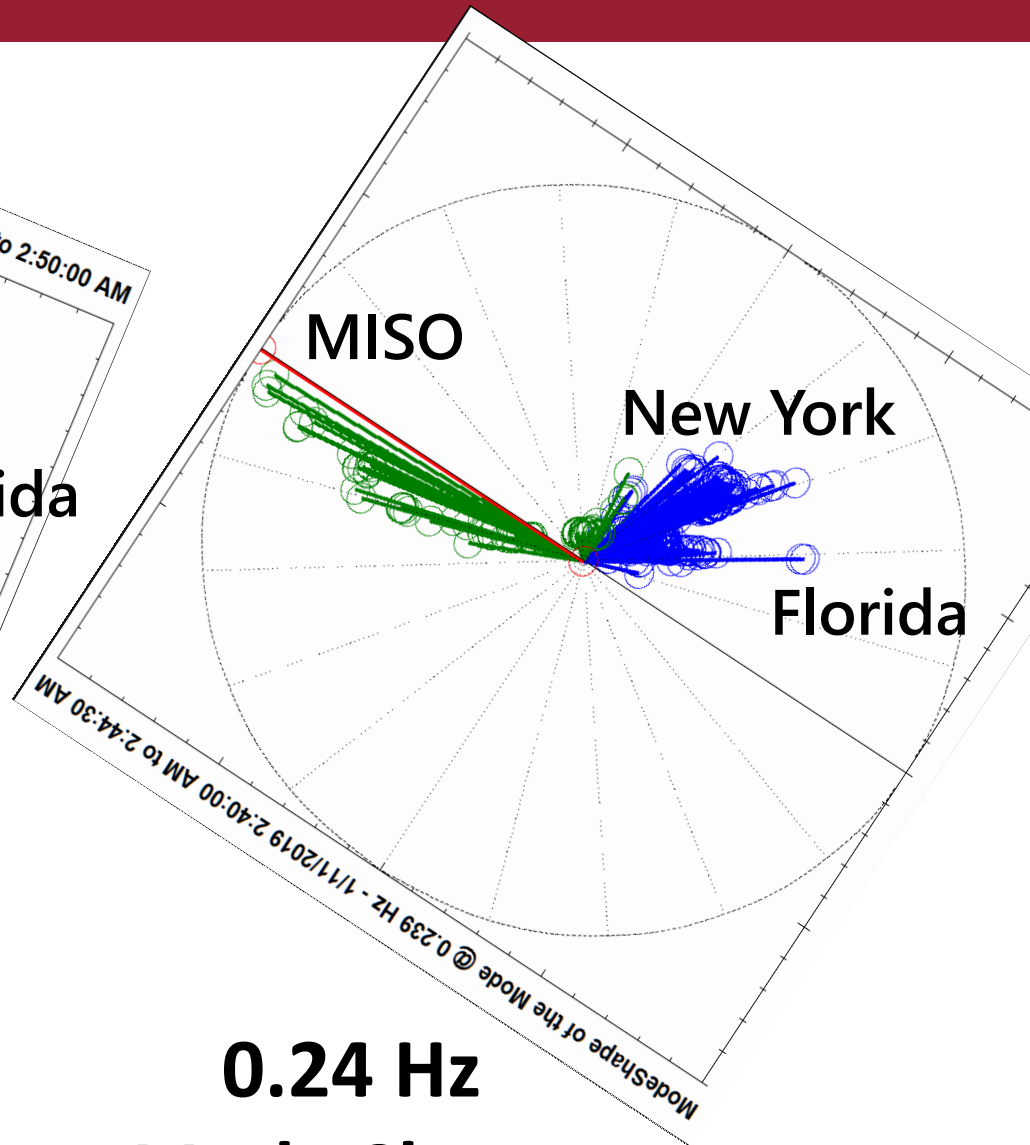
Florida

MISO, MB

# Contribution from Two Modes

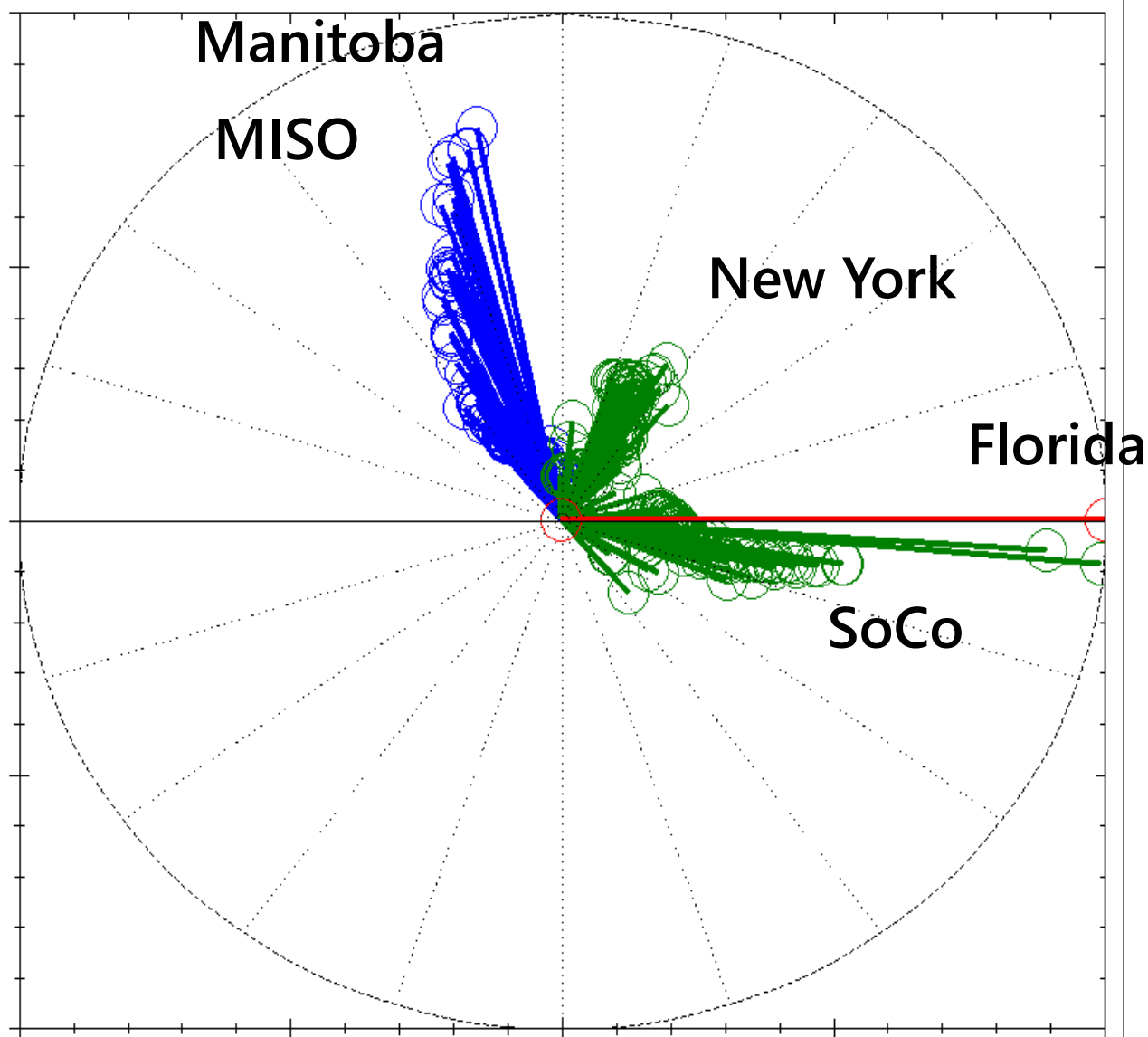


**0.3 Hz Oscillation  
Shape**



**0.24 Hz  
Mode Shape**

# 0.25 Hz Oscillation Shape



**Oscillation Response is the net effect from 0.24 Hz and 0.3 Hz modes.**

# Resonance effects from modes

- Several modes may get excited.  
What we see is the net effect.
- Mode shapes of dominant modes known =>  
We can estimate modal amplifications of  
system modes from analysis of PMU  
measurements.
- Resonance effect from each mode can be  
estimated by LSE formulation.
- Counteractions and controls.